

Thermal performance characteristics of passively cooled 1.3 μ m InGaAsN/GaAs double quantum well lasers

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- Generic device description
- Description of the laser model
- Numerical experiments
- Conclusions

Generic device structure:

QW material: InGaAsN

Number of QWs: 2

Bulk material: AlGaAs

Device length: $L = 250 \mu\text{m}$

Device width: $W = 50 \mu\text{m}$

Ridge width: $W_r = 2 \mu\text{m}$

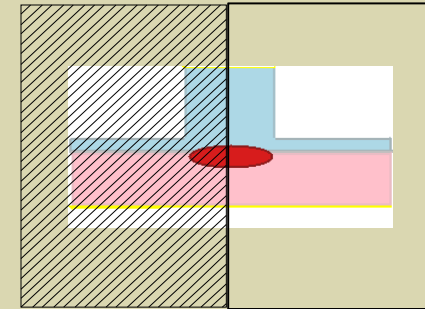
Front facet reflectivity: $R_f = 0.3$

Back facet reflectivity: $R_b = 0.7$

Heat sink resistance: $R_{hs} = 1.0 \text{ K/W}$

Front facet output power: $P_{out} = 10 - 15 \text{ mW}$

AlGaAs thermal conductivity: $\kappa = 10 - 40 \text{ Wm}^{-1}\text{K}^{-1}$



Simulation conditions:

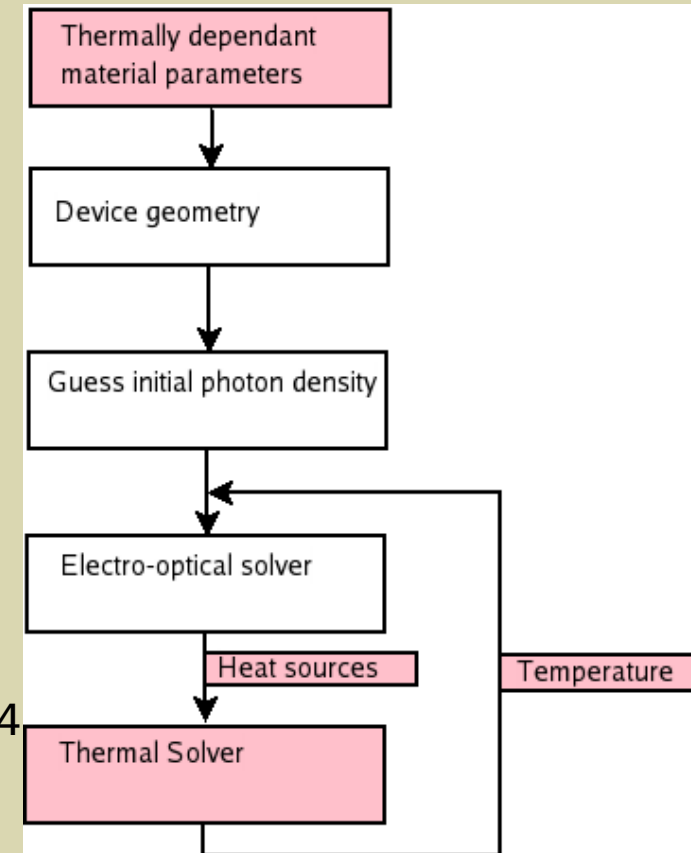
- All simulations performed in 2D
- Half-space simulations used to reduce computation time
→ Possible because of device symmetry

Electrical Model

- Bipolar 1D - 2D Drift Diffusion (DD) model (0th and 1st moments of the Boltzmann Transport Equation (BTE))
 - Includes thermal driving terms in current equation
- Poisson's equation
- QW capture/escape equations for each QW
- 2D lattice heat equation solved in external solver

Optical Model

- Photon rate equation interacting with all QWs
- Gain and spontaneous emission calculated using a 4x4 band ***k.p*** method



All equations solved using Newton's method



Thermally dependent parameters

- Electron and hole mobilities
- Band gap
- Electron affinity
- Gain (through look up table)
 - Fermi-Dirac statistics
- Spontaneous emission
- SRH recombination
- Auger recombination
- Effective densities of states
- Thermal lattice conductivity
- Maxwell-Boltzmann statistics
- Heat capacity

Heat sources

- Shockley-Read-Hall
- Auger recombination
- Free carrier absorption
- Spontaneous emission
- Joule heating
- Peltier cooling/heating

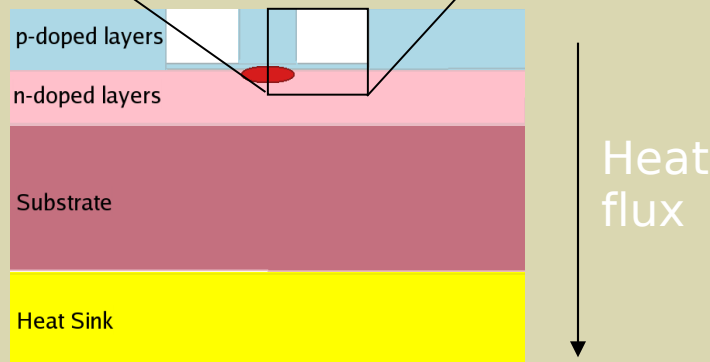
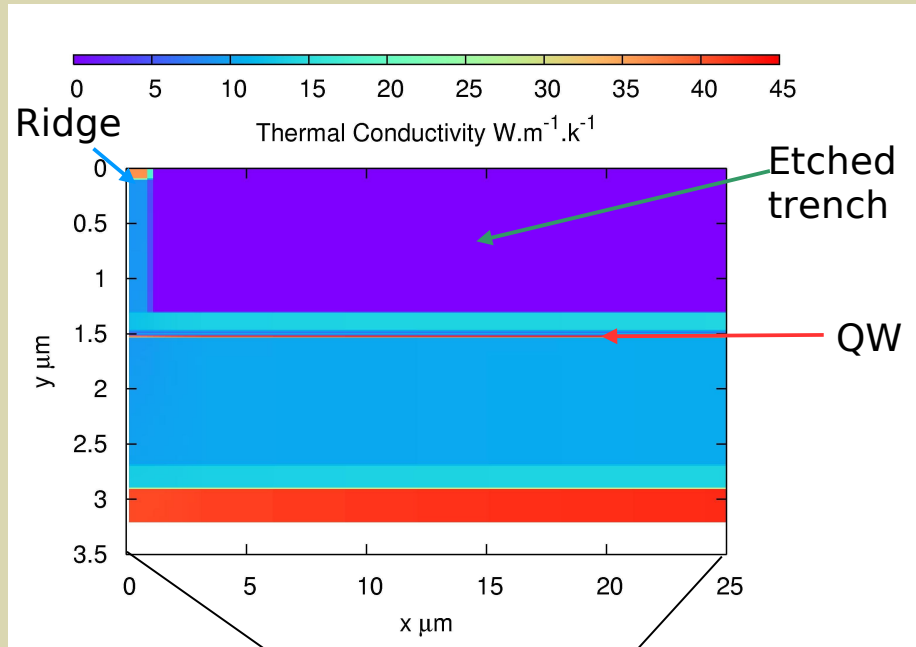
Meshing

- Separate electrical and thermal meshes
 - Mesh same over electrical region (avoids interpolation)
 - Electrical problem area small compared to thermal problem area
- Software updated to simulate p-side up/down mounting

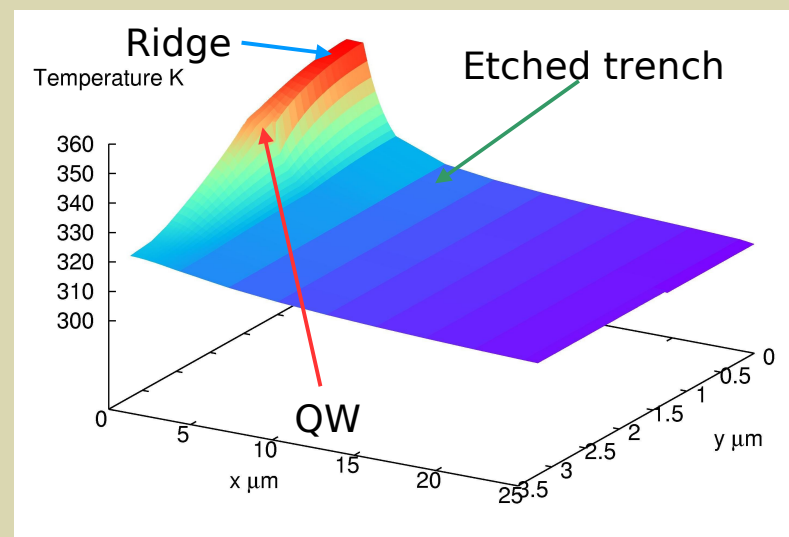
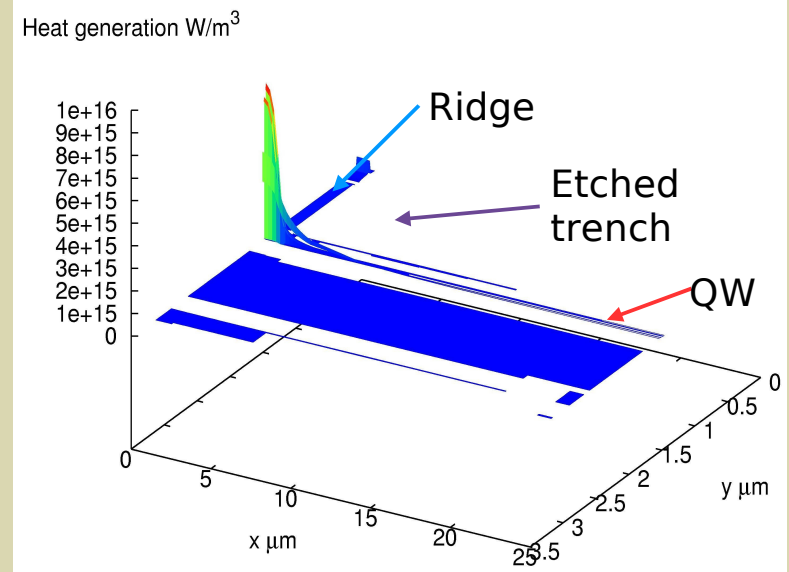
Typical thermal simulation - p-side up mounting



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Can this be improved upon?



1. Ridge width

- How does ridge width affect the thermal performance?

2. Trench width

- How does etch trench width affect thermal performance?

3. Trench filling

- Can we improve device performance by filling the trenches?

4. Investigation of poor thermal environments

- How do external temperature variations affect device performance?

5. Mounting p-side up/down

- How does substrate thickness affect p-side up mounted devices?

6. Meshing

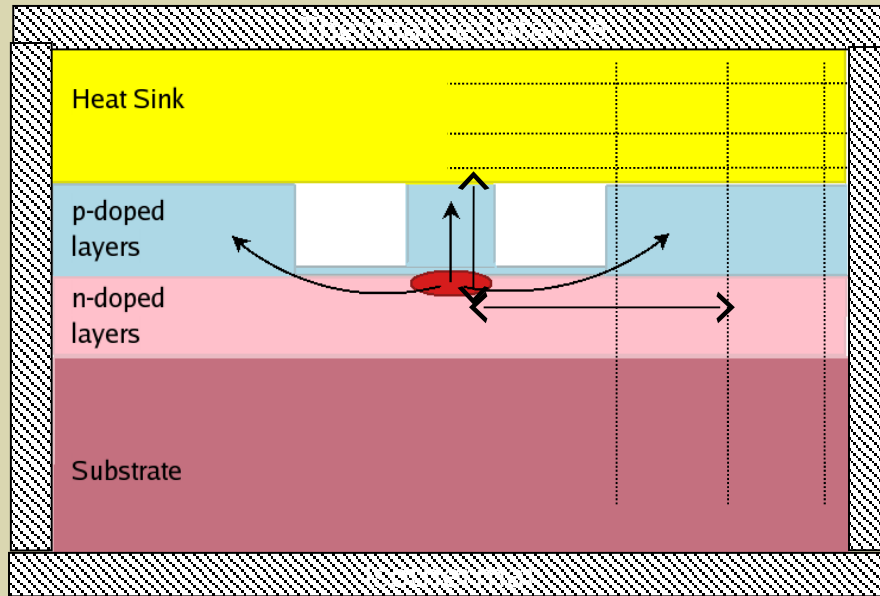
- How far does the thermal mesh need to extend beyond the electrical mesh?

Thermal simulation window & boundary conditions

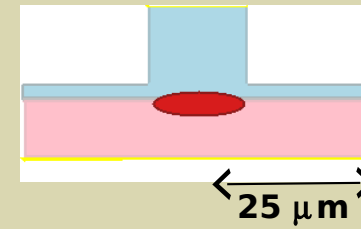


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Thermal mesh



Electrical mesh

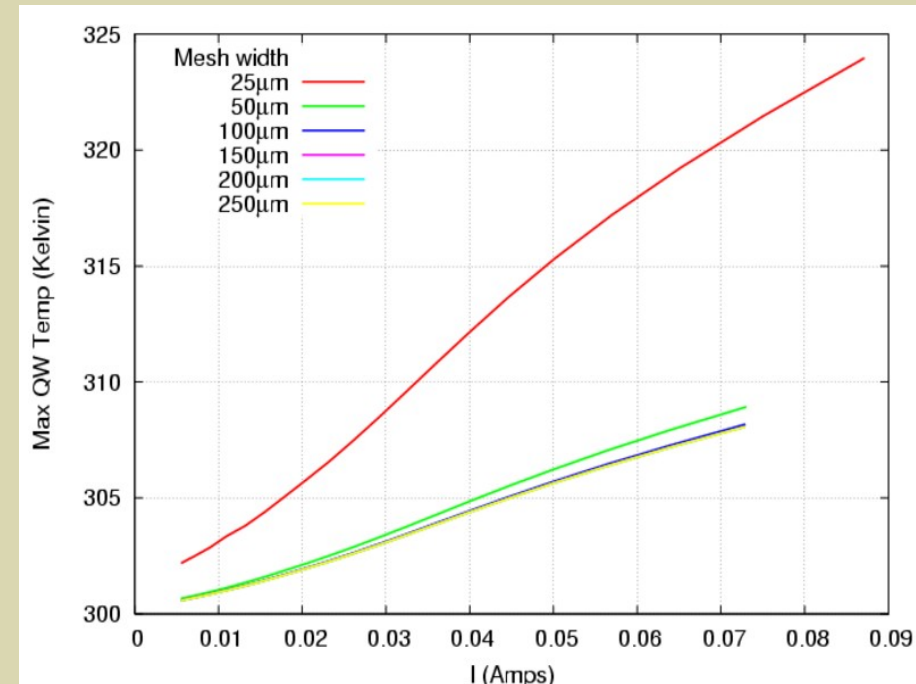


Q. How wide does the thermal mesh need to be?

A. About 4 times wider than the electrical mesh
Most important for p-side down mounting

Q. How far does the vertical mesh need to extend into the heat sink to model thermal spreading?

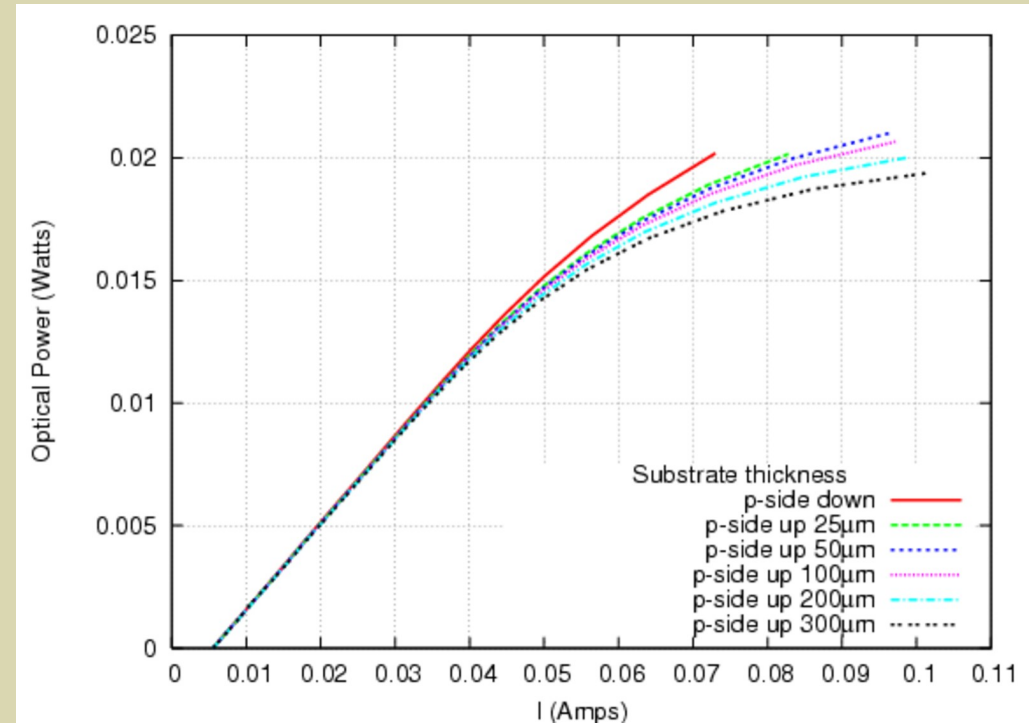
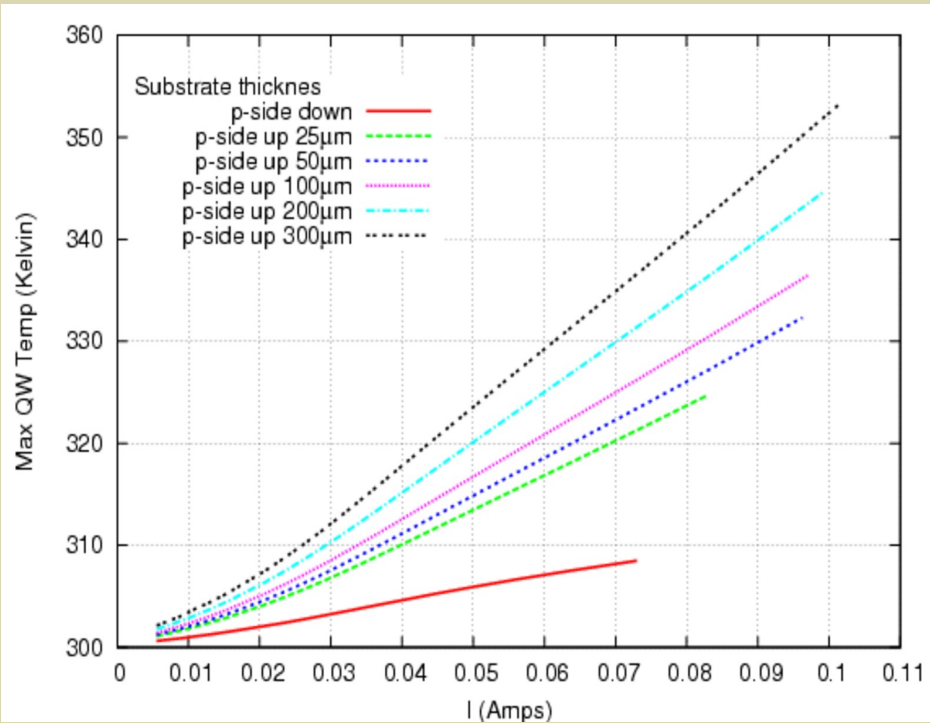
A. 100μm



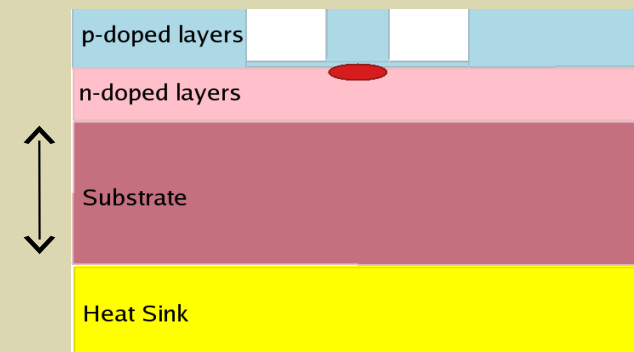
Impact of substrate height on maximum temperature



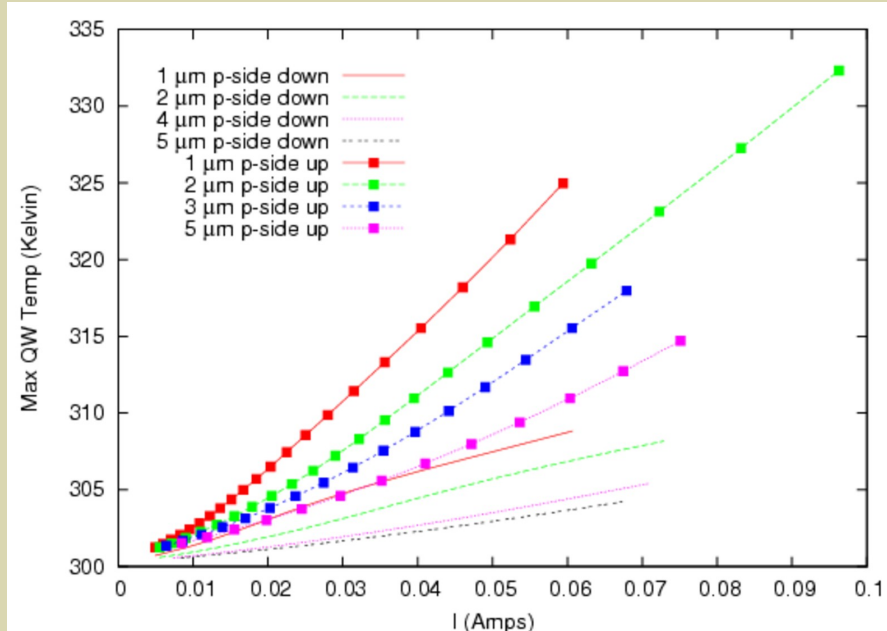
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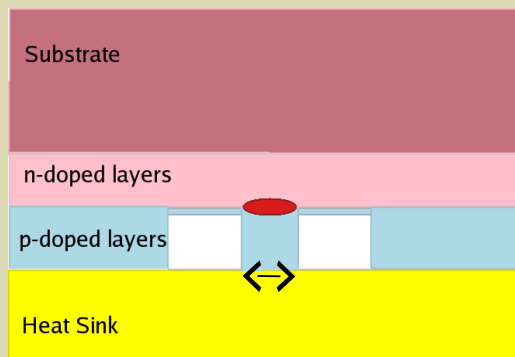
- Better high frequency response for p-side up mounts
 - What is the thermal penalty?
- Reducing substrate thickness reduces:
 - QW temperature
 - The onset of thermal rollover



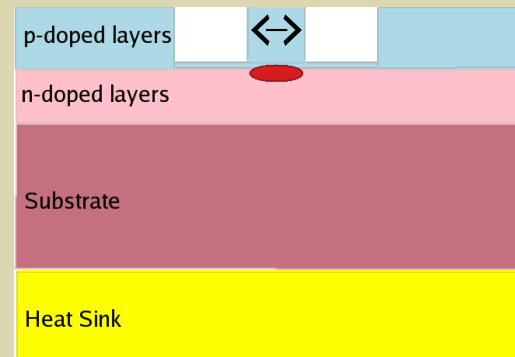
Variation of ridge width



- How does the ridge width affect the QW temperature?
- What is the impact of p-side up mounting on this?
- Wider ridge → higher electrical conductivity → less Joule heating
- Wider ridge → bigger area → lower heat flux density → lower temperature
- P-side up mounting → no route for heat to escape up the ridge → higher QW temperature
- The ridge forms a *thermal island* that gets very hot



P-side down

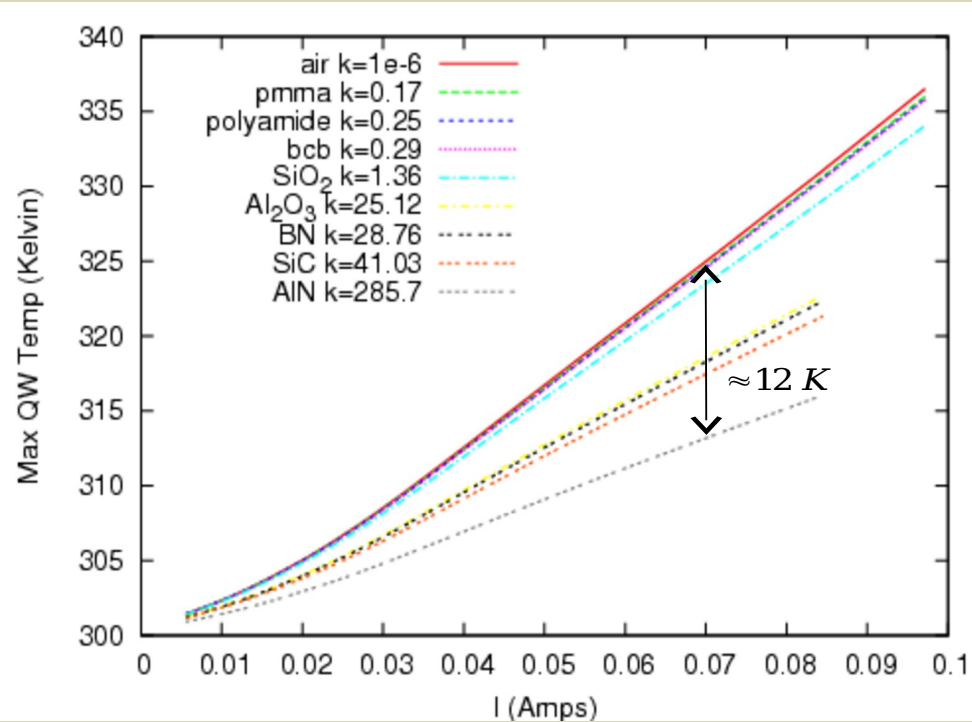


P-side up

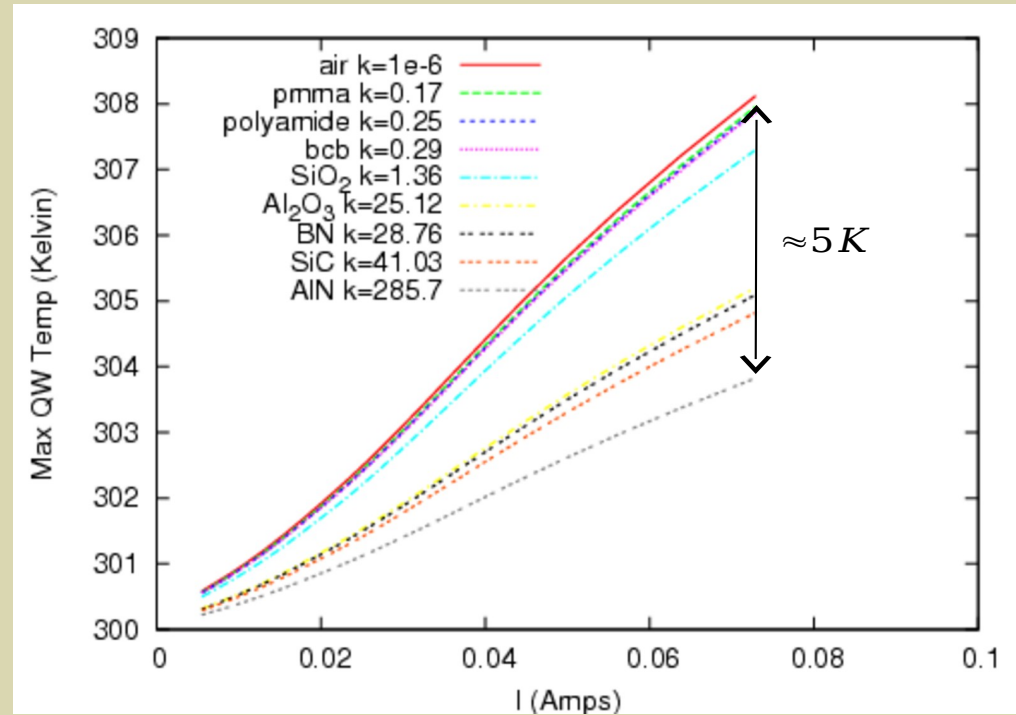
Thermal conductivity of the etched trench



P-side up



P-side down

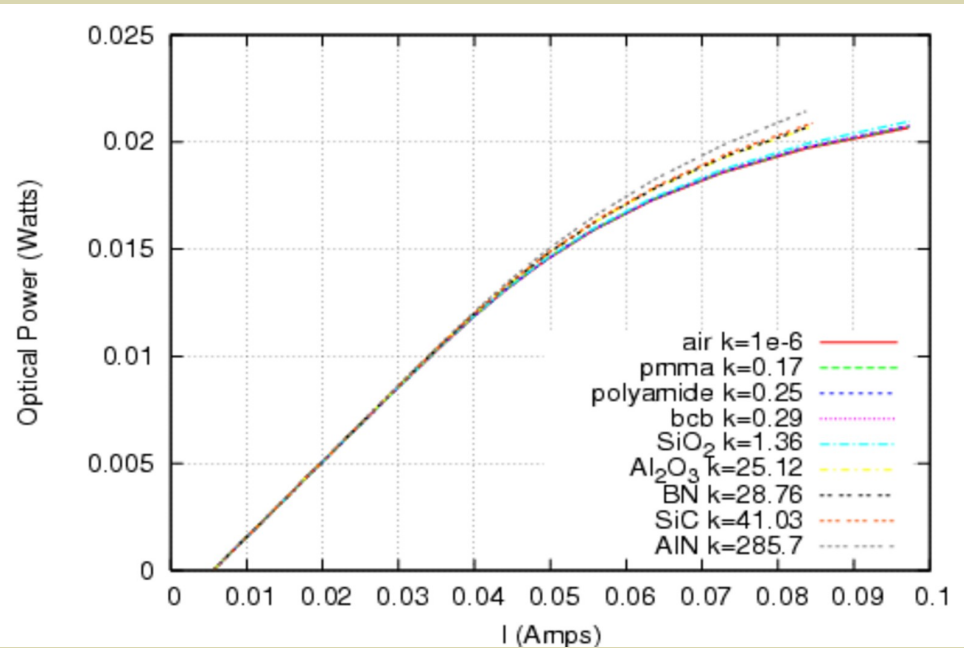


- Material system makes a *large* impact for p-side up mounted devices
- Less impact for p-side down mounting

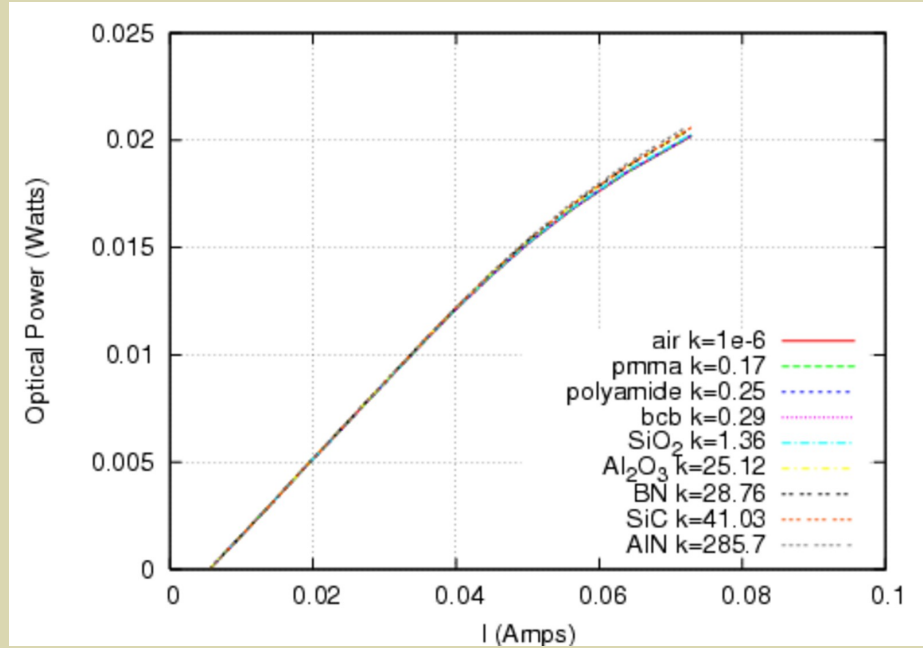
Thermal conductivity of the etched trench



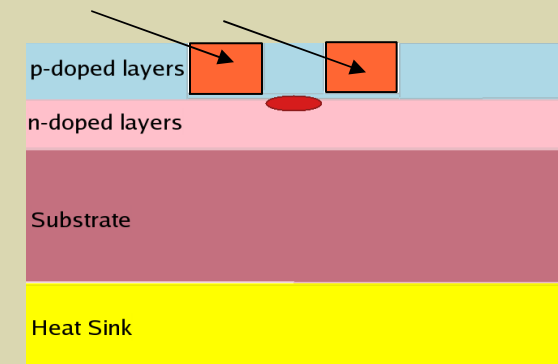
P-side up



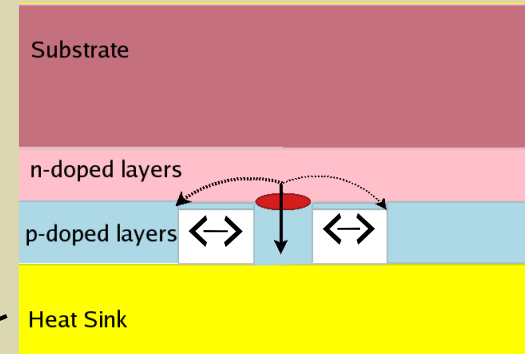
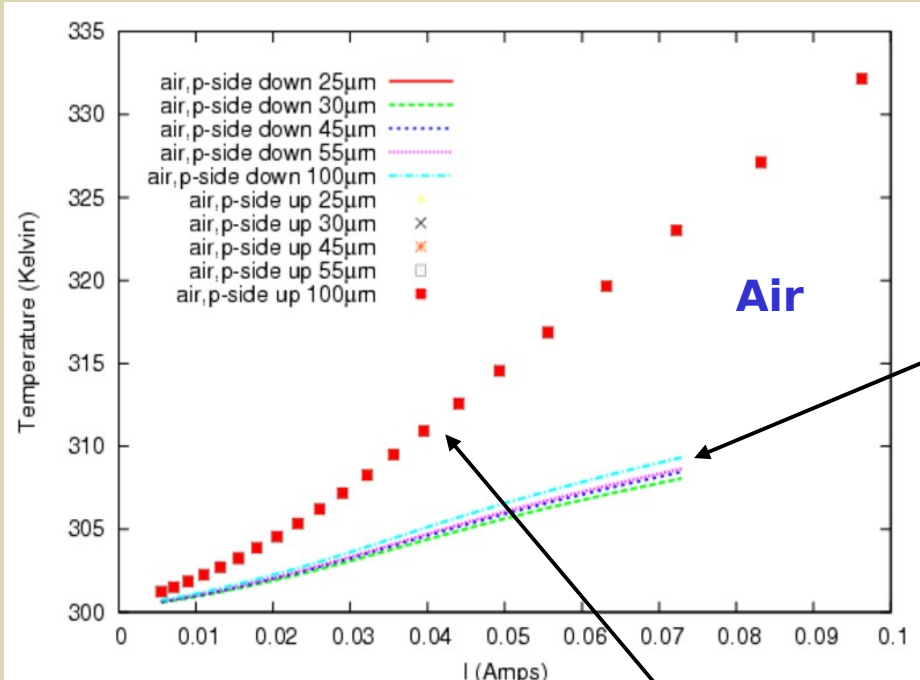
P-side down



- The change in temperature can be seen in the L-I curves
- Thermal roll-over in L-I curve due to temperature dependence of gain



Variation of etch trench width

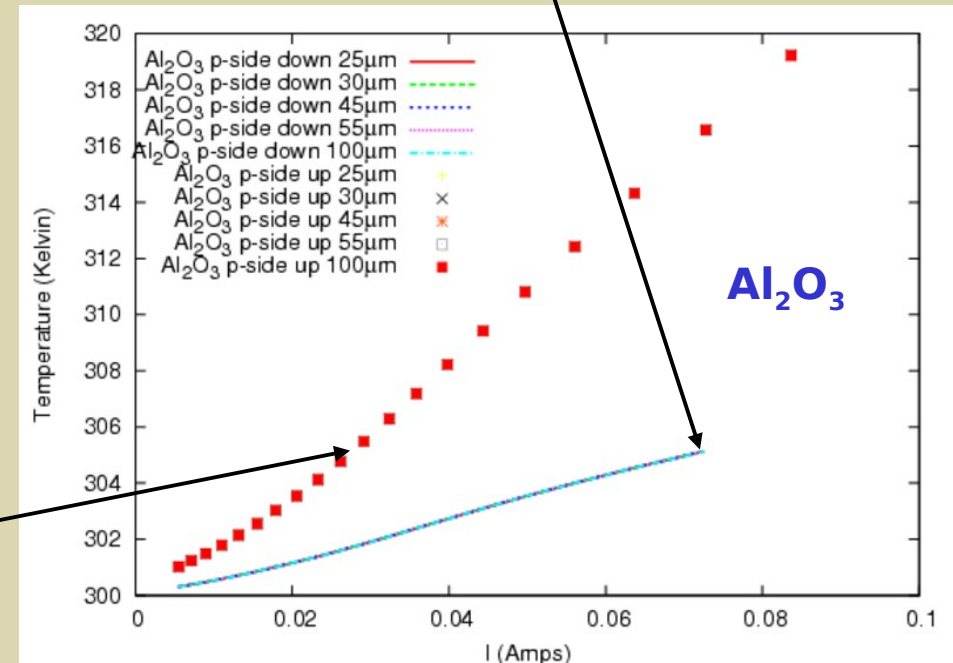
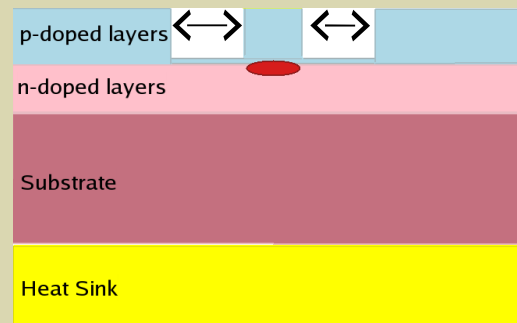


P-side down

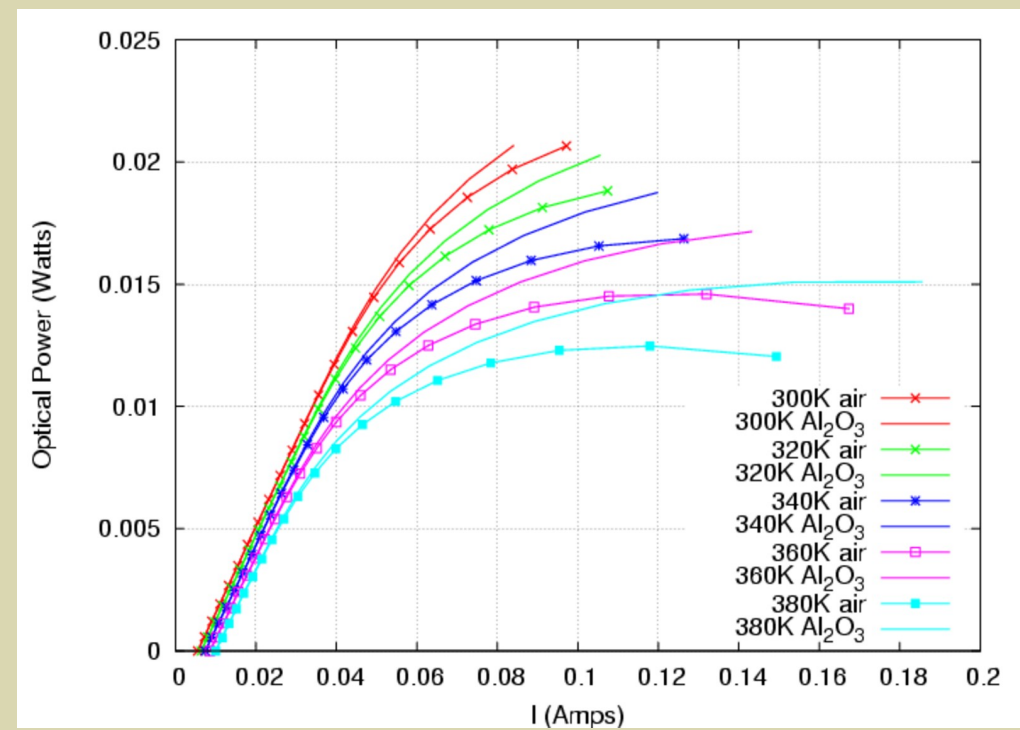
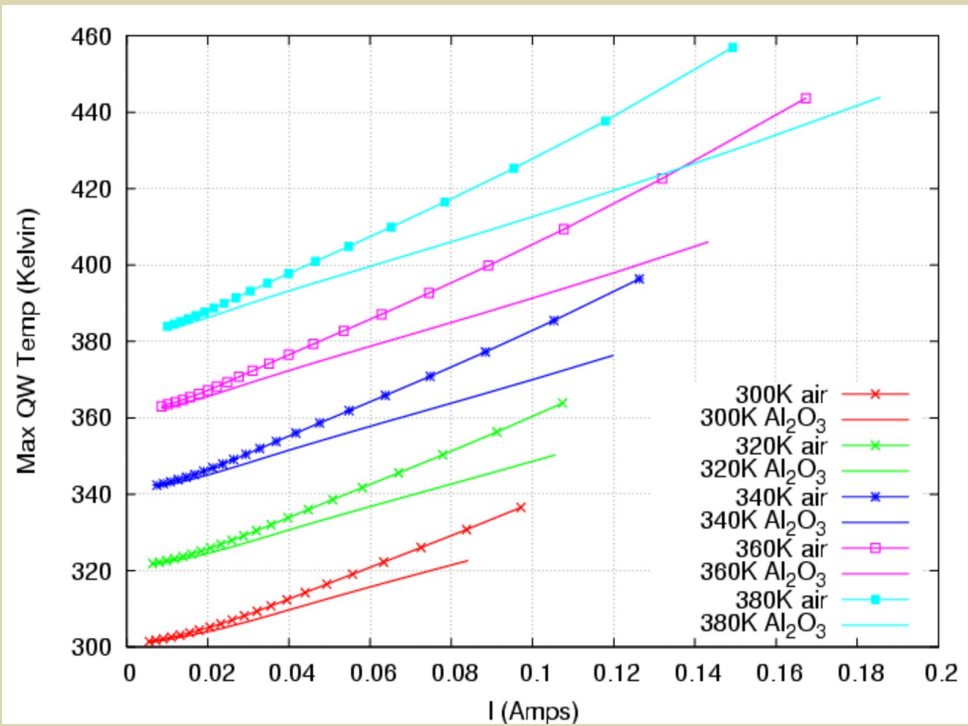
- Cooler
- Etched trenches block heat flow out of device

P-side up

- Hotter
- Etched trenches block/help heat flow from ridge



Operation at elevated temperature



- Devices often operate in a poor thermal environment → increased heat sink temperatures
- Filled etched trenches at high temperatures → significant performance improvements
- Operating temperature strongly affects device reliability and life time

- The thermal mesh should extend $100\mu\text{m}$ laterally beyond the etched trenches and $100\mu\text{m}$ vertically into the heat sink
- There is a significant thermal penalty for p-side up mounting
- A thinner substrate results in a lower QW temperature
- Refilling the trenches with a thermally conductive material significantly reduces the QW temperature.
- A wider ridge reduces electrical resistance
 - Reduces Joule heating and decreases the thermal series resistance of the ridge
 - For a single-mode device, there is a limit to how wide the ridge can be
- The design of uncooled lasers requires the global optimisation of their thermal, electrical and optical performance (usually requiring a trade-off).

Thank you for your attention



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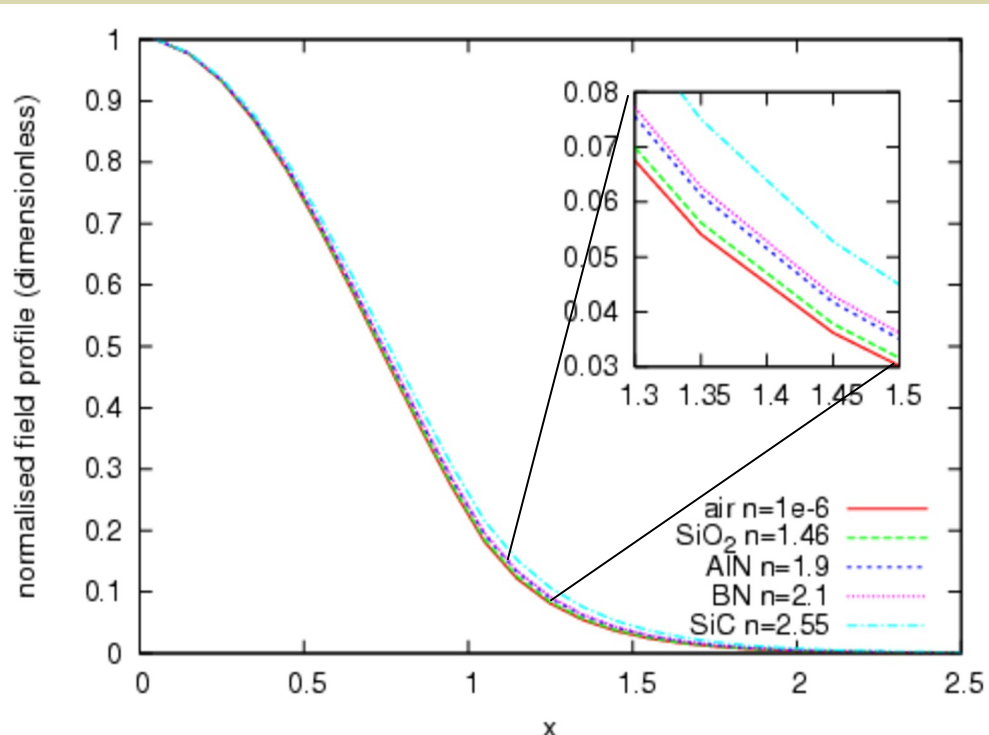
What are the optical penalties of filling the trenches?



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- More poorly confined lateral mode
 - Slightly worse confinement factor (minimal)
 - However this loss is more than compensated for by improved thermal performance

Ridge width = $2\mu\text{m}$



Trend: The larger the refractive index of the trench, the worse the guiding

With decrease in index step and width of etch leaky modes are more likely to cause problems